

# **Geometry and the Imagination**

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An academic exercise presented in partial fulfillment for the degree of  
Bachelor of Science with Honours in Applied Mathematics.

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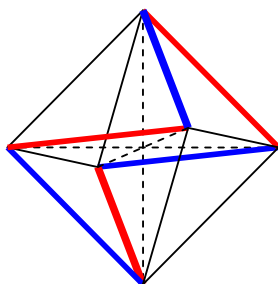
## Acknowledgements

I would like to thank my supervisor, A/P Aslaksen, for conducting this wonderful project. I am grateful to him for his time and his patience with me. I benefit greatly from discussions I have had with him on this project, and I hereby express my appreciation for his guidance full of inspirations. This project has been a meaningful and pleasant experience with excitements and joys of discoveries, which I will always remember.

I would like to dedicate the regular octahedron shown below to my lovely girlfriend, Goose. To me, she is as nice and perfect as a regular octahedron.

I would like to dedicate the space hexagon highlighted in bold on the regular octahedron to all the people who have been kind to me. I would like to share my joys with you all.

I would like to dedicate the hyperboloid of one sheet that contains all six sides of the space hexagon to my parents. I would like to express my gratitude to them for their love to me over the years. Something is behind the scene, silent and invisible, yet you know.



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## Summary

This thesis begins with discussions of properties of second order plane curves and quadratic surfaces in Chapter I. In the study of quadratic surfaces, the concepts of “surfaces of revolution” and “ruled surfaces” are introduced. As a particular example, the surface of the hyperboloid of revolution of one sheet is closely examined by the author. After showing that a hyperboloid of revolution of one sheet can be obtained by rotating a straight line in space, the author goes on to examine the properties of the straight lines lying in the surface. Following that the author extends these properties to the hyperboloid of one sheet of the most general type. This process gives rise to a new concept, called a “strain”. It is a transformation in space which can deform surfaces of revolution to general type surfaces.

In Chapter II, the author examines the concept of “strain” and explores the properties of this kind of transformation in space. When exploring the properties, the author notices that strain transformations preserve collinearity, concurrency as well as tangency. From this, the author points out the connection between the idea of perspectives in projective geometry and the nature of strain transformations. As a demonstration, the author concludes that if we can prove Brianchon’s theorem in the circle case, we will get the ellipse case “for free”, by using an argument based purely on the properties of strain transformation.

In Chapter III, two interesting problems are discussed. In the first problem, the author presents a proof for the fact that given any 3 skew straight lines in space which are not parallel to a common plane, there always exists a hyperboloid of one sheet containing these three lines. The basic idea of the author's proof is to find some strain transformations that can transform the given 3 lines into positions such that a known hyperboloid of one sheet contains all 3 of them. Due to the arbitrariness and ambiguity of the positions of the three given straight lines, it proved difficult to determine such strain transformations. In the author's method of finding the desired transformations, a very special space hexagon is constructed from the three given straight lines, and from this, the author finishes the rest of the proof using properties of strain transformations.

In the proof of the first problem in chapter III, the author has a close look at the structure of the regular octahedron, and discovers that the structure of the regular octahedron can be used to visualize the connections between the face-centered cubic lattice packing and the face-centered hexagonal lattice packing when constructing the closest regular packing of spheres in space. This interpretation of the author's is explained in the second problem which concludes this thesis. □

## **Author's Contributions**

All proofs from Chapter I onwards presented in this thesis are new proofs worked out by the author. Among these new proofs, the author is most proud of his proof for the fact that given any three skew straight lines which are not parallel to a common plane, there always exists a hyperboloid of one sheet containing them. This proof is presented in section 3.1.

The properties of strain transformations presented in section 2.3 are summarized by the author. The proof presented in section 2.3 for the fact that strain transformations in space preserve the type of a quadratic surface is worked out by the author.

The interpretations in section 3.2 on the closest regular packing of spheres using the structure of the regular octahedron are due to the author.

All the figures in this thesis are drawn by the author.

# Introduction

*“In mathematics, as in any scientific research, we find two tendencies present. On the one hand the tendency toward **abstraction** seeks to crystallize the logical relations inherent in the maze of material that is being studied, and to correlate the material in a systematic and orderly manner. On the other hand, the tendency toward **intuitive understanding** fosters a more immediate grasp of the objects one studies, a live rapport with them, so to speak, which stresses the concrete meaning of their relations.*

*“As to **geometry**, in particular, the abstract tendency has led to the magnificent systematic theories of Algebraic Geometry, of Riemannian Geometry, and of Topology; these theories make extensive use of abstract reasoning and symbolic calculation in the sense of algebra. Notwithstanding this, it is still as true today as it ever was that intuitive understanding plays a major role in geometry. And such concrete intuition is of great value not only for the research worker, but also for anyone who wishes to study and appreciate the results of research in geometry.*

*“It is possible in many cases to depict the geometric outline of the methods of investigation and proof, without necessarily entering into the details connected with the strict definitions of concepts and with the actual calculations.”*

*----David Hilbert (1932), preface to “**Geometry and the Imagination**” [4]*

The main scope of this project is to study the book “*Geometry and the Imagination*” by *David Hilbert* and *S. Cohn-Vossen*. This book, which was written some 70 years ago, is, according to Hilbert, intended to “give a presentation of geometry in its visual and intuitive aspects”. In light of this statement, readers of this book indeed find that a great number of interesting geometric problems in this book are dealt with solely by means of visual imagination instead of abstract algebraic calculations. Take the following

problem from Hilbert's book for example:

A plane not at right angles to the axis of a circular cylinder nor parallel to it intersects the cylinder in a plane curve (Figure I-1A). Prove that the curve of intersection is an ellipse.

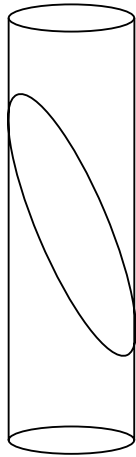


Figure I-1A

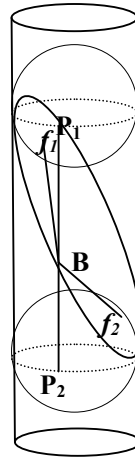


Figure I-1B

Instead of building up a Cartesian coordinate system and proving this result analytically, the proof given in Hilbert's book is as simple as follows: Imagine we take two spheres which just fit in the cylinder and put these two spheres inside the cylinder so that each of the two spheres touches the cylinder in a circle. We then move them within the cylinder until they touch the intersecting plane from opposite sides at points  $f_1$  and  $f_2$  (Figure I-1B). Let  $\mathbf{B}$  be any point on the curve of intersection of the plane and the cylinder, we take the straight line through point  $\mathbf{B}$  lying on the cylinder (i.e. parallel the axis). Suppose the straight line meets the circles of contact of the spheres at two points  $\mathbf{P}_1$  and  $\mathbf{P}_2$ .

$\mathbf{Bf}_1$  and  $\mathbf{BP}_2$  are tangents to a fixed sphere through a fixed point  $\mathbf{B}$ , and all such tangents must be of the same length, because of the rotational symmetry of the sphere. Thus  $\mathbf{Bf}_1 = \mathbf{BP}_2$ ; similarly  $\mathbf{Bf}_2 = \mathbf{BP}_1$ . It follows that

$$\mathbf{Bf}_1 + \mathbf{Bf}_2 = \mathbf{BP}_1 + \mathbf{BP}_2 = \mathbf{P}_1\mathbf{P}_2$$

Again by rotational symmetry, the distance  $\mathbf{P}_1\mathbf{P}_2$  is a constant independent of point  $\mathbf{B}$  on the curve. Therefore  $\mathbf{Bf}_1 + \mathbf{Bf}_2$  is constant for all points  $\mathbf{B}$  on the curve, so the curve of intersection is an ellipse with foci at  $f_1$  and  $f_2$ .  $\square$

The six chapters of this book covered a wide diversity of materials dealing with interesting problems from various branches of geometry. I shall now list down the titles of the six chapters of Hilbert's book, they are,

Chapter 1 The simplest curves and surfaces

Chapter 2 Regular systems of points

Chapter 3 Projective configurations

Chapter 4 Differential geometry

Chapter 5 Kinematics

Chapter 6 Topology

Due to time constraint, in this project, I have only been working on the first 3 chapters of this book, namely on simplest curves and surfaces, on regular systems of points and on projective geometry. All problems discussed in this thesis arise from study in these branches of geometry; there are no discussions on topology or differential geometry.

The content of this thesis is not a repeat of what Hilbert wrote in his book. There is no point to discuss what have already been clearly explained in that book because the book itself is a well-written book. My purposes of this thesis are as follows,

To apply methods used in the book to solve problems not discussed in the book; (e.g. Section 1.1).

To give my own explanations and interpretations on the results and ideas which I found interesting; (e.g. Section 3.2)

To provide proofs where I feel necessary but the book omitted. (e.g. Section 3.1).

Before I move on to Chapter I, I have to say here that “*Geometry and the Imagination*” is a wonderful book that gives me inspirations. I admire the spirit in this book of using imagination to sense out visual intuitive natures of geometric problems. I recommend the book to those who have not read it, and who like to use their imagination.

## Chapter I

# The Simplest Curves and Surfaces

### §1.1 Properties of second order plane curves

If we do not consider degenerate cases and imaginary curves, there are three types of second order plane curves. They are the parabola, the hyperbola, and the ellipse (circles are categorized as a special case of the ellipse). In this section I will discuss two selected problems on properties of second order plane curves.

#### Optics properties of the Hyperbola

Second order plane curves exhibit several interesting properties, among which, they share analogous properties in optics. Take a hyperbola (Figure 1.1-1) for example,

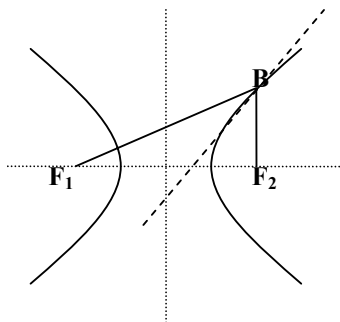


Figure 1.1-1

Given the property that  $||F_1B| - |F_2B||$  is constant for any point  $B$  on a hyperbola with

foci  $F_1$  and  $F_2$ , it can be derived that the straight line segments  $BF_1$  and  $BF_2$  make the same angle with the tangent to the hyperbola at  $B$ . Thus any light ray originating at  $F_2$  and reflected in the hyperbola will appear to emanate from  $F_1$ . To see why this is so, I shall first derive the following lemma.

**Lemma 1.1** Let  $F_1$  and  $F_2$  be two fixed points located on different sides of a straight line  $p$  (Figure 1.1-2). For all the points on  $p$ , if point  $B^*$  gives the function  $||F_1B| - |F_2B||$  the maximum value, then  $p$  bisects  $\angle F_1B^*F_2$ .

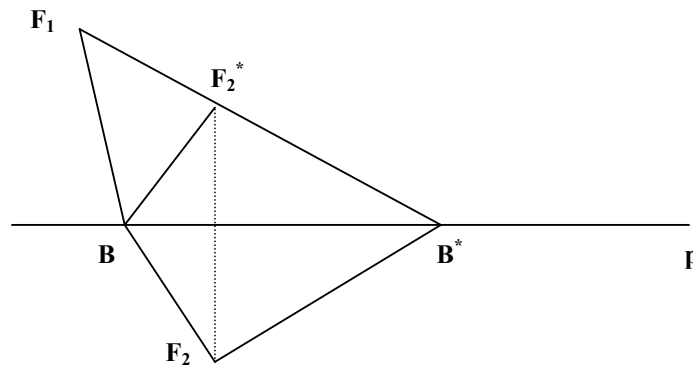


Figure 1.1-2

Proof for Lemma 1.1. Take the mirror image of  $F_2$  with respect to line  $p$ , denote the image point with  $F_2^*$ . Since the case when  $F_1$  and  $F_2^*$  coincide is trivial, here we assume they are distinct. For any point  $B$  on  $p$ , we have  $|F_2B| = |F_2^*B|$ . Suppose the line connecting  $F_1$  and  $F_2^*$  intersects  $p$  at point  $B^*$ . Since  $F_1$ ,  $F_2^*$  and  $B^*$  are collinear, we have

$$||F_1B^*| - |F_2^*B^*|| = |F_1F_2^*|$$

For any other point  $\mathbf{B}$  distinct from  $\mathbf{B}^*$  on  $\mathbf{p}$ ,  $\mathbf{F}_1$ ,  $\mathbf{F}_2^*$  and  $\mathbf{B}$  form a triangle, by the property of a triangle we have

$$\|F_1\mathbf{B}\| - \|F_2^*\mathbf{B}\| < \|F_1F_2^*\|$$

Hence for any point  $\mathbf{B}$  on  $\mathbf{p}$ ,  $\mathbf{B} = \mathbf{B}^*$  gives  $\|F_1\mathbf{B}\| - \|F_2^*\mathbf{B}\|$ , or  $\|F_1\mathbf{B}\| - \|F_2\mathbf{B}\|$  the maximum value. Since  $F_2^*$  is the mirror image of  $F_2$  about  $\mathbf{p}$ , we have  $\angle F_2^*\mathbf{B}^*\mathbf{B} = \angle F_2\mathbf{B}^*\mathbf{B}$ , or  $\angle F_1\mathbf{B}^*\mathbf{B} = \angle F_2\mathbf{B}^*\mathbf{B}$ .  $\square$

In general, for any point  $\mathbf{B}_1$  in between the two branches of a hyperbola,  $\mathbf{B}_2$  on the hyperbola and  $\mathbf{B}_3$  outside the area bounded by the two branches of hyperbola we have

$$\|F_1\mathbf{B}_1\| - \|F_2\mathbf{B}_1\| < \|F_1\mathbf{B}_2\| - \|F_2\mathbf{B}_2\| < \|F_1\mathbf{B}_3\| - \|F_2\mathbf{B}_3\| \quad \dots(*)$$

This fact can be understood by constructing a family of hyperbolas having the same pair of foci, and the fact that none two curves of this family intersect.

Since a tangent line of a second order curve has no point in common with the curve other than the point of contact, it follows that any tangent line to a hyperbola must lie entirely in between the two branches of the hyperbola. Thus from (\*) we see that, among all the points on the tangent in Figure 1.1-1, point  $\mathbf{B}$  gives  $\|F_1\mathbf{B}\| - \|F_2\mathbf{B}\|$  the maximum value, by lemma 1.1, the tangent bisects  $\angle F_1\mathbf{B}F_2$  and hence the result.

## The parabola as a conic section

Second order plane curves are also called conic sections, or simply conics, for the simple reason that they can be obtained by intersecting a plane with a circular cone in proper ways. In this section I will present a proof for the following fact:

A plane parallel to one and only one generating line of a circular cone intersects the cone in a parabola.

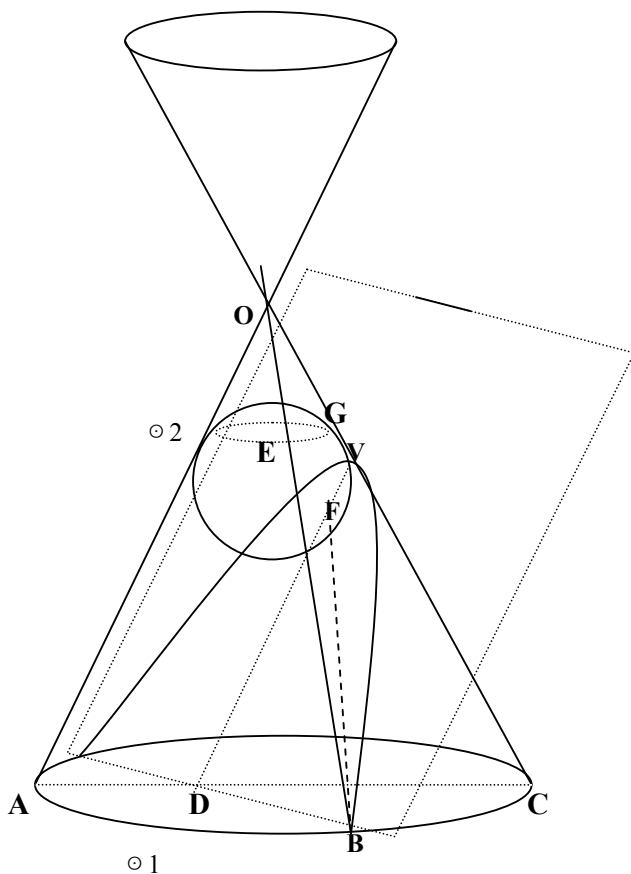


Figure 1.1-3A

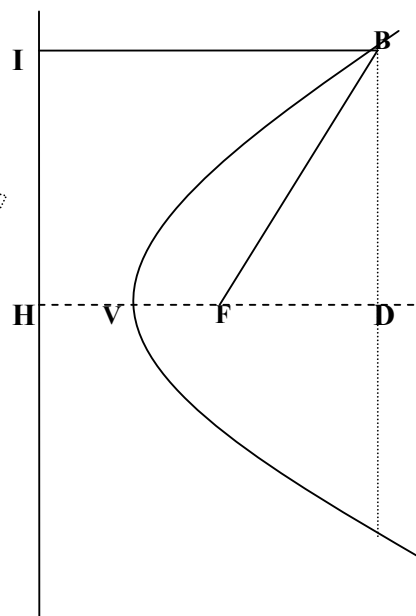


Figure 1.1-3B

In Figure 1.1-3A, a plane perpendicular to the axis of the cone intersects the cone in a

circle  $\odot 1$ , let **A** and **C** be two points on the circle such that they are on the same diameter of  $\odot 1$ . We now take a plane parallel to **OA**, this plane intersects the cone in a curve that we are interested in. By our assumption, the intersecting plane can only be parallel to exactly one generating line of the cone, which is **OA** in our case, it can be shown that this plane is perpendicular to the plane containing  $\triangle \mathbf{OAC}$ . Suppose the inclined plane intersects  $\odot 1$  at point **B**, intersects **OC** at point **V**, and intersects **AC** at point **D**, intuitively the curve of intersection is symmetric about **VD**.

We now put a sphere inside the cone which touches the cone in a circle  $\odot 2$  and the inclined plane at point **F**. (Note this is always possible, and the intersection of the angle bisectors of  $\angle \mathbf{AOC}$  and  $\angle \mathbf{OVD}$  coincides the center of the sphere.) Note also that **F** must be a point on **VD** by symmetry.

Suppose **OB** intersects  $\odot 2$  at point **E**, and **OC** intersects  $\odot 2$  at point **G**. Since **BE** **BF** are two tangents to a fixed sphere through a fixed point, **BE** **BF** must be equal in length, so we have

$$\mathbf{BE} = \mathbf{BF};$$

For the same reason,

$$\mathbf{VG} = \mathbf{VF}.$$

Since **OA** = **OC**, and **VD** // **OA**, so we have

$$\mathbf{VD} = \mathbf{VC};$$

By rotational symmetry we have

$$\mathbf{BE} = \mathbf{GC}.$$

From the above three equalities, it follows that

$$\mathbf{BF} = \mathbf{BE} = \mathbf{GC} = \mathbf{VG} + \mathbf{VC} = \mathbf{VF} + \mathbf{VD} \quad \dots(*)$$

We now consider (\*) on the intersecting plane, refer to Figure 1.1-3B. We have

$$\mathbf{BF} = \mathbf{VF} + \mathbf{VD},$$

if we extend  $\mathbf{DV}$  to a point  $\mathbf{H}$  such that  $\mathbf{VH} = \mathbf{VF}$  and we then draw the perpendicular line to  $\mathbf{VD}$  with foot at point  $\mathbf{H}$ , we see that now,  $\mathbf{BF} = \mathbf{HD}$ , if  $\mathbf{BI}$  is the distance from  $\mathbf{B}$  to the line we draw, then

$$\mathbf{BF} = \mathbf{BI}.$$

By the directrix definition of a parabola, we see that the curve of intersection is indeed a parabola with focus at  $\mathbf{F}$ .  $\square$

## §1.2 Surfaces of revolution

In previous discussions, I have mentioned the circular cylinder and the circular cone. The circular cylinder is the simplest curved surface. It can be obtained by rotating a straight line about an axis parallel to it. Because of this, the circular cylinder is called a surface of revolution. Surfaces of revolution are surfaces that can be generated by rotating a plane curve about an axis lying in the plane of the curve. The generating plane curve is called the generator of the surface. From the definition of surfaces of revolution, we see that a circular cone is also a surface of revolution. It can be obtained by rotating a straight line about an axis intersecting it. In Figure 1.1-3A, the straight line through **OA** is a generator of the cone and it intersects the axis of the cone at point **O**.

In either of the cases of a circular cylinder or a circular cone, we have rotated a straight line about another straight line that lies in a common plane with the first one. Now one question arises, if we have two skew straight lines in space, and we rotate one about another, what kind of surface we will get? It seems that the surface in question may not be a surface of revolution, because it violates the condition that the generator must be a plane curve lying in the same plane with the axis of revolution, while in our case, two skew lines never lie in the same plane. But as it turns out, if we have two skew straight lines in space and we rotate one about another, the surface we get is a hyperboloid of revolution of one sheet! And this particular type of hyperboloid is a surface of revolution because it can be obtained by rotating a hyperbola about one of its axes of

symmetry. In the following section, I will examine the above-mentioned beautiful result.

### The Hyperboloid of revolution of one sheet

In Figure1.2-1A, suppose the hyperbola in the **ZOY** plane has the following equation

$$Y^2/a^2 - Z^2/b^2 = 1 \quad (a, b > 0)$$

Its two asymptotes then can be expressed as

$$Z = \pm (b/a) Y$$

These two asymptotes make the same angle  $\theta$  with **Z** axis, and

$$\theta = \tan^{-1}(a/b)$$

If we rotate the curve about **Z** axis, we will get a surface of revolution shown in Figure1.2-1B. It is a special case of a general hyperboloid of one sheet, the plane **XOY** or any other plane parallel to **XOY** always intersects the surface in a circle.

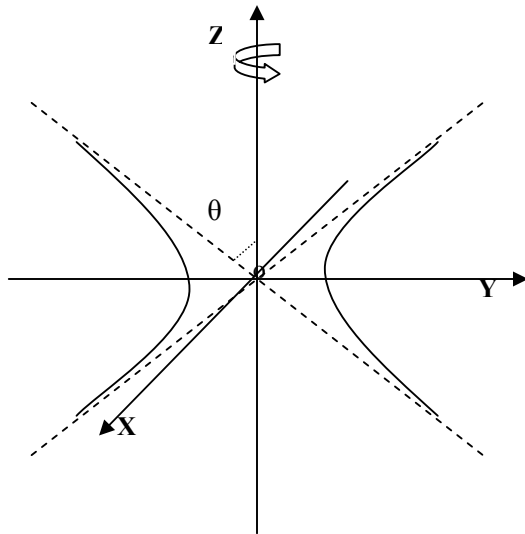


Figure1.2-1A

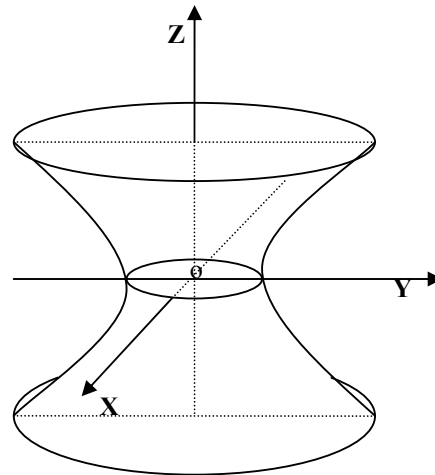


Figure1.2-1B

We call this kind of surface the hyperboloid of revolution of one sheet. It can be represented by the following equation:

$$X^2/a^2 + Y^2/a^2 - Z^2/b^2 = 1$$

If we move one of the asymptotes of the hyperbola in Figure 1.2-1A along the **X** axis by a distance of **a**, keeping the line intersecting **X** axis and parallel to its initial position in the course, we will get a straight line skew to the **Z** axis as shown in Figure 1.2-1C. Now the interesting fact is that, if we rotate this skew line about **Z** axis, we will get a surface (Figure 1.2-1D) which is identical to the hyperboloid of one sheet as shown in Figure 1.2-1B!

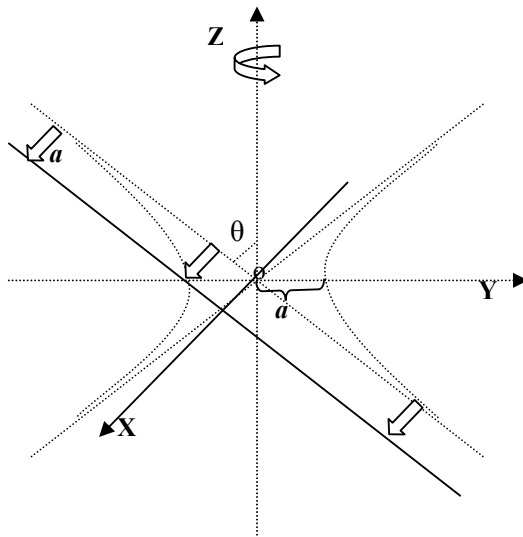


Figure 1.2-1C

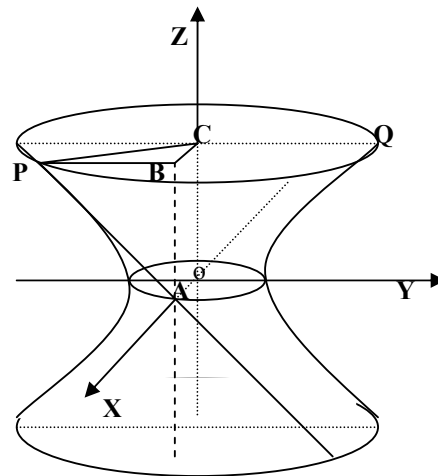


Figure 1.2-1D

To see this result, take any point **P** on the skew line, consider the plane containing **P** and parallel to the **XOY** plane. Suppose this plane intersects the **Z** axis at point **C** and

intersects either branch of the hyperbola at point **Q**, I shall show that  $\mathbf{CP} = \mathbf{CQ}$ . In other words, by rotating point **P** about the **Z** axis, when **P** hits the **YOZ** plane, it will hit on the hyperbola.

In Figure 1.1-1D, suppose **A** is the intersection of the skew line with **X** axis. We take point **B** in the plane which contains **P** and parallel to the **XOY** plane such that  $\mathbf{AB} // \mathbf{OC}$ .

If the distance from point **P** to **XOY** plane is  $\mathbf{Z}_0$ , then

$$\mathbf{AB} = \mathbf{OC} = \mathbf{Z}_0$$

By our assumption,  $\angle \mathbf{PAB} = \theta = \mathbf{Tan}^{-1}(a / b)$ , we have

$$\mathbf{PB} = \mathbf{AB} \mathbf{Tan}(\theta) = \mathbf{AB} (a/b) = \mathbf{Z}_0 (a/b)$$

It is easy to see that **BCOA** forms a parallelogram, therefore

$$\mathbf{BC} = \mathbf{AO} = a$$

It can be shown that **BC** is perpendicular to the plane containing **A B P**, and hence  $\mathbf{BC} \perp \mathbf{PB}$ , it follows that

$$\mathbf{PC} = \sqrt{(\mathbf{PB}^2 + \mathbf{BC}^2)} = \sqrt{[\mathbf{a}^2 + \mathbf{Z}_0^2 (a^2/b^2)]}$$

Suppose by rotating **P** about **Z** axis, **P** will be brought to a point **Q** with coordinates ( 0,  $\mathbf{Y}_0$ ,  $\mathbf{Z}_0$  ) in the **ZOY** plane, from above calculation, we see that

$$\mathbf{Y}_0 = |\mathbf{PC}| = \sqrt{[\mathbf{a}^2 + \mathbf{Z}_0^2 (a^2/b^2)]}$$

Or equivalently,

$$Y_0^2/a^2 - Z_0^2/b^2 = 1$$

By comparing the above equation to that of the original hyperbola, we see that point **Q** must be a point on the hyperbola! Since **P** is arbitrarily chosen on the skew line, and for any point **Q** on the hyperbola there is a one-to-one such corresponding point **P**, this completes the proof.  $\square$

### §1.3 Ruled surfaces

In the previous section, we see that if we rotate a straight line about an axis skew to it, we will get a hyperboloid of revolution of one sheet, thus this kind of one sheeted hyperboloid can be generated by sweeping a straight line along a circle in space in a particular manner. In general, a surface that can be generated by moving a straight line along a certain fixed course is called a ruled surface. By this definition, we see that hyperboloids of revolution of one sheet are ruled surfaces, and so are circular cylinders and circular cones. All these surfaces contain infinitely many straight lines in them.

But, as ruled surfaces, our hyperboloid of revolution of one sheet is distinguished from circular cylinders and cones by the special property that each point of the surface is on more than one of the straight lines lying in the surface. Because of this, the hyperboloid of revolution of one sheet is also called a doubly ruled surface, while cylinders and cones do not belong to this category.

To see why a hyperboloid of revolution of one sheet is a doubly ruled surface, we look at the symmetrical properties of the two asymptotes of the hyperbola we have considered in previous section as shown in Figure 1.2-1C. It can be shown that choosing either one of the two asymptotes, they always generate the same surface. In fact the two resulting hyperboloids of revolution of one sheet coincide.

Hence we see that there are two families of straight lines on the hyperboloid of revolution of one sheet, the two families are distinguished by the property that any two straight lines belonging to the same family can be brought onto each other by a rotation about the axis of the surface. Observe from our construction that, each of the two families covers the hyperboloid of one sheet completely, thus any point on the surface lies on two straight lines, each of which comes from a different family.

Figure 1.3-1 shows the two families of straight lines on a hyperboloid of revolution of one sheet.

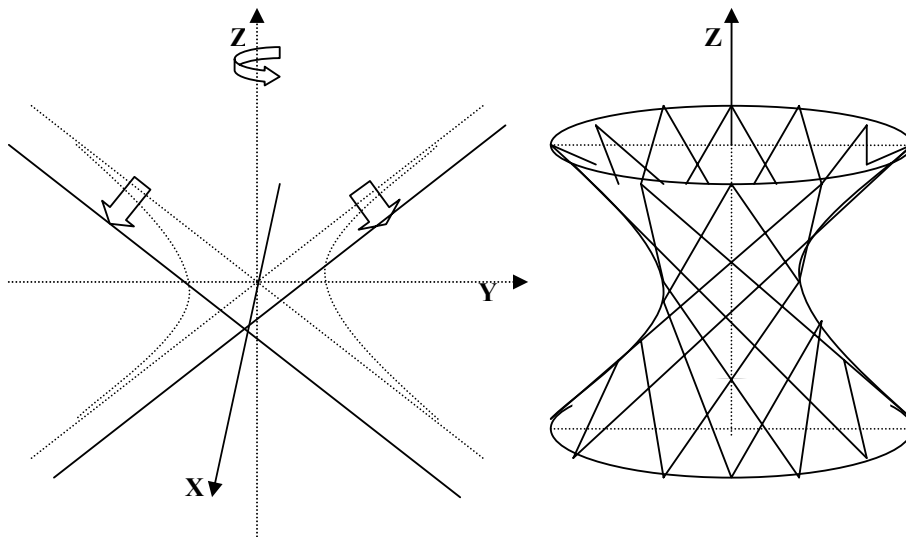


Figure 1.3-1

There is an interesting property about these two families of straight lines, viz., every straight line of one family intersects every straight line of the other family (or is parallel to it), but any two lines of the same family are mutually skew.

To see this result, we consider the circular cylinder generated by moving the smallest circle on the hyperboloid along the rotation axis of the surface. It is easily seen that all the straight lines on the surface are tangent to this cylinder, and the points of contacts form the smallest circle on the hyperboloid, denote this circle with  $\odot_1$ . If we now choose two straight lines  $p$  and  $q$  on the surface each from a different family (Figure 1.3-2), I shall now show that they either intersect or are parallel.

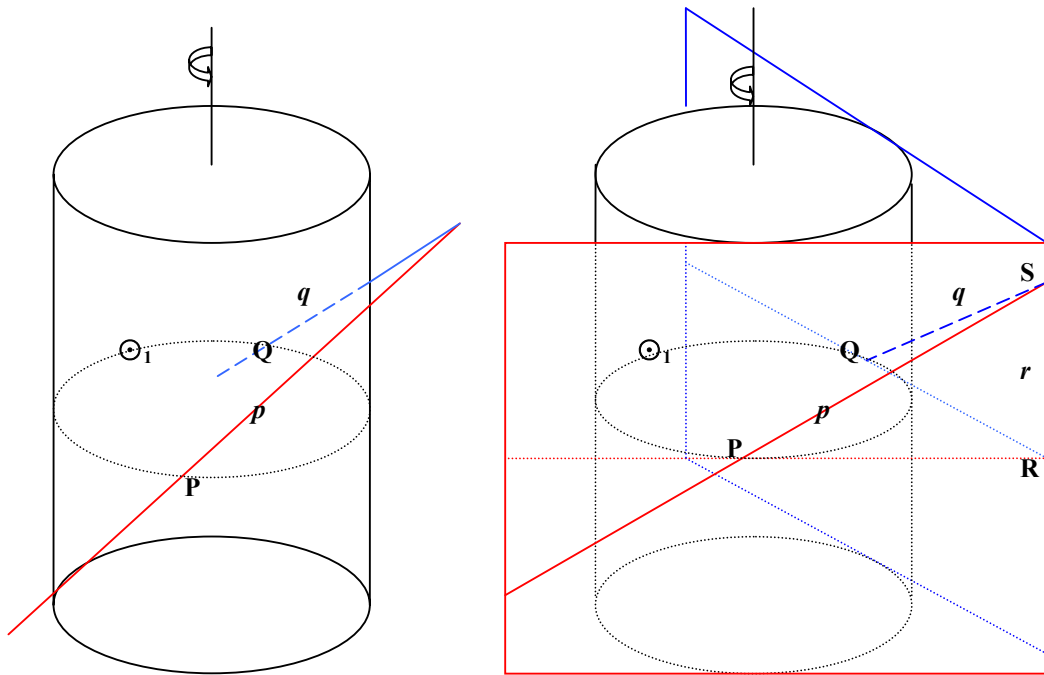


Figure 1.3-2

Suppose  $p$  and  $q$  touch the cylinder at points  $P$  and  $Q$  respectively. Assume  $P$  and  $Q$  are two distinguished points on  $\odot_1$ . We now draw the two tangents to  $\odot_1$  at points  $P$  and  $Q$  on the plane that contains  $\odot_1$ , if they are parallel, then it is easily seen that  $p \parallel q$ . Assume these two tangents meet at point  $R$ , we have  $RP = RQ$ .

Suppose the plane contain line  $p$  and tangent to the cylinder intersects the corresponding plane for  $q$  intersects in a straight line  $r$ , point  $R$  must be a point on  $r$ , and further more,

$$r \perp RP \text{ and } r \perp RQ.$$

Suppose  $p$  intersect  $r$  at  $S_1$  and  $q$  intersect  $r$  at  $S_2$ , we see that

$$S_1R = RP \tan (\angle S_1PR)$$

$$S_2R = RQ \tan (\angle S_2QR)$$

Since we have shown that  $RP = RQ$ , and by the symmetrical properties of the two family of straight lines we have  $\angle S_2QR = \angle S_1PR$ , it follows that  $S_1R = S_2R$ .

Thus  $S_1$  and  $S_2$  must coincide, and can be denoted by one point, say  $S$ , it follows that  $p$   $q$  intersect at point  $S$ . If  $p$  and  $q$  have been chosen such that they belong to the same family, we see from Fig1.3-2 that in this case  $S_1$  and  $S_2$  never coincide, because apparently point  $R$  must lie in between them. So any two lines from the same family must be mutually skew.

As mentioned at the beginning of the above arguments, when the two planes containing  $p$  and  $q$  and tangent to the cylinder are parallel, or equivalently, points  $P$  and  $Q$  are on the same diameter of  $\odot_1$ ,  $p$  and  $q$  are parallel instead of intersecting. In fact, for any straight line  $p$  belonging to one family of the straight lines, there is one and only one straight line  $q$  from the other family such that these two lines are parallel instead of intersecting. This seemingly trivial case turns out to be great importance in solving the problem to be discussed in section §3.1.  $\square$

## Chapter II

# Strain Transformations

### §2.1 Hilbert's dilatation

The hyperboloid of revolution of one sheet obtained by rotating a hyperbola or a straight line does not give us a general type of hyperboloid of one sheet. We see the difference by comparing the standard equations of the two in the Cartesian coordinate system.

Hyperboloid of revolution of one sheet has the following standard equation,

$$X^2/a^2 + Y^2/a^2 - Z^2/c^2 = 1 \quad (a, c > 0) \quad \dots(1)$$

While the equation for the general type of hyperboloid of one sheet is

$$X^2/a^2 + Y^2/b^2 - Z^2/c^2 = 1 \quad (a, b, c > 0) \quad \dots(2)$$

Apparently in the equation of the surface of revolution, the two coefficients of the terms  $X^2$  and  $Y^2$  are the same, while this condition need not be satisfied for the general type.

Despite this, we can always get the general type of the hyperboloid of one sheet from a hyperboloid of revolution of one sheet by a deformation called “dilatation” (so called by Hilbert). This is achieved by holding fixed all the points of some arbitrary plane containing the axis of rotation and moving all other points in a fixed direction toward the plane or away from it in such a way that the distances from the plane of all points in

space change in a fixed ratio.

I shall now demonstrate the concept of “dilatation” by deforming the surface represented by equation (1) to the surface represented by (2) described above.

In (1) we have,

$$\mathbf{X}^2/a^2 + \mathbf{Y}^2/a^2 - \mathbf{Z}^2/c^2 = 1 \quad (\mathbf{a}, \mathbf{c} > 0) \quad \dots(1)$$

If we now let

$$\mathbf{X}' = \mathbf{X},$$

$$\mathbf{Y}' = (\mathbf{a} / \mathbf{b}) \mathbf{Y}, \quad (\mathbf{b} > 0) \text{ and}$$

$$\mathbf{Z}' = \mathbf{Z}$$

We then have

$$\mathbf{X}'^2/a^2 + \mathbf{Y}'^2/b^2 - \mathbf{Z}'^2/c^2 = 1 \quad (\mathbf{a}, \mathbf{b}, \mathbf{c} > 0) \quad \dots(3)$$

We see that we get equation (3) from (1) by introducing some special  $\mathbf{X}'$   $\mathbf{Y}'$  and  $\mathbf{Z}'$  which rescales the original coordinate system. Intuitively, the meaning of introducing  $\mathbf{X}'$   $\mathbf{Y}'$  and  $\mathbf{Z}'$  can be understood as follows: originally we have a surface of revolution with equation (1), we now fix the  $\mathbf{XOZ}$  plane, and move all the points not in the  $\mathbf{XOZ}$  plane along directions parallel to the  $\mathbf{Y}$  axis in such a way that the distances from all points to the  $\mathbf{XOZ}$  plane change by a factor of  $\mathbf{a} / \mathbf{b}$ . In this process, all the points on our original surface are moved to new positions which now form a general hyperboloid of one sheet having equation (2).

In Hilbert's book, he points out that it can be proved that such a transformation of "dilatation" changes all circles into ellipses (or circles), straight lines into straight lines, planes into planes, and all second-order curves and surfaces into second-order curves and surfaces respectively.

Hilbert does not point out explicitly that, in general, "dilatations" in space always preserve the type of second order curves or surfaces located at any position in space! Take a hyperboloid of revolution of one sheet for example, not only can we choose the fixed plane to be a plane containing the axis of revolution of the hyperboloid, in fact we can choose any plane we like to be the fixed plane, and do "dilatations" as many times as we like using different fixed planes, the resulting surface, after all these deformations, will always remain as a hyperboloid of one sheet. It will never be deformed into any other types of surface like a hyperboloid of two sheets or a hyperbolic paraboloid, and of course, neither will it become a surface that has an irregular shape that we do not know of the type. This result will be explained in the following sections when I explore more on the properties of dilatations.

## §2.2 Dilatations, shears, strains and linear transformations

Before I set out to explore the properties of the deformation of “dilatation” mentioned in previous section, I think there is a need to do some clarifications about the terminology used here.

In Hilbert’s book, he uses the term “dilatation” to mean the following deformation in space:

Holding fixed all the points of a plane and moving all other points in a fixed direction toward the plane or away from it in such a way that the distances from all points in space to the fixed plane change in a fixed (nonzero) ratio.

In my first draft of this thesis, I followed Hilbert’s terminology. Whenever I came to the above-mentioned deformation, I always referred it as the “dilatation”. But then my supervisor, Helmer, points out that this terminology tends to be old-fashioned, modern definition for the term “dilatation” seems to be different from what Hilbert described in his book.

It is not surprising to see that the terminology used in Hilbert’s book tend to be old-fashioned considering the fact that the book was written more than 70 years ago. Later I consulted G. Martin [5] and J. Cederberg’s [2] books and learnt that, there are a number of rather confusing concepts similar to Hilbert’s concept of “dilatation”. They

are “dilation”, “central dilation”, “similarity”, “central similarity”, “shear” and “strain”. These terminologies are used in the past and nowadays to define different kinds of transformations in the plane or in space. To avoid any confusion, I shall draw a diagram which shows explicitly the meanings of some of the above-mentioned terms and the time these meanings were used.

Meaning \ Time	Old-fashioned terms	Modern terms
Transformation Type I	Dilatation	Dilation
Transformation Type II	Dilation	Central dilation / Central similarity

Table 2.2-1

In Table 2.2-1, Transformation of Type I represents a transformation in space such that any straight line is transformed into a straight line parallel to it. Transformation of Type II can be understood as the following process: holding a fixed point **P** in space, for any other point **Q** distinct from **P**, we move **Q** along the straight line connecting **P** and **Q** in such a way that the distance between them changes in a nonzero fixed ratio.

Nowadays, central dilation and central similarity have the same meaning. Both of them represent Transformation of Type II. The term “similarity” alone is a transformation such that the distances between any two points are changed by a fixed ratio. If we adapt

ourselves to the modern terms, there are three theorems on these concepts in the plane:

Theorem I: A dilation is either a translation or a central dilation/central similarity.

(Martin, p.139)

Theorem II: A similarity is a product of a central dilation and an isometry. (Martin, p.139) An isometry is a transformation that preserves distances. In the plane, there are four types of isometry: translations, rotations, reflections and glide reflections.

Theorem III: A nonidentity similarity is exactly one of the following: isometry, stretch, stretch rotation, stretch reflection. (Martin, p.141) Here a stretch means a central dilation of positive ratio. A stretch rotation is a composition of a stretch and a rotation with the center of rotation coinciding the fixed point of the stretch.

We see from Table 2.2-1 that in the past people use the term “dilatation” to denote transformations of type I. Note that even used in this way, the term “dilatation” in the table have a different meaning from Hilbert’s concept. Hilbert’s “dilatation” clearly is not a transformation of type I because it does not in general transform straight lines to parallel positions, so the term “dilatation” does not seem to be a good terminology to denote Hilbert’s concept of “dilatation”. So in the following discussions, I shall just call it “Hilbert dilatation”. Incidentally, in Martin’s book, he uses the term “strain” to define a very close concept to Hilbert dilatation.

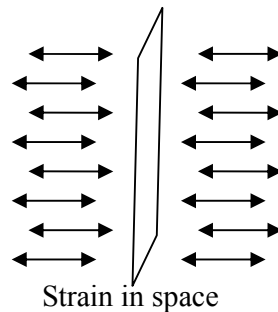
A **strain** in the plane means that we fix a straight line in the plane, and move all points

not on this line along directions perpendicular to this fixed line in such a way that the distances from all points to this fixed line change in a nonzero fixed ratio. In Cartesian coordinate system, a strain of ratio  $k$  about the  $X$ -axis (with  $Y$ -axis as the fixed straight line) can be represented by the following set of equations,

$$\begin{cases} X' = kX \\ Y' = Y \end{cases} \quad \text{Where} \quad k \neq 0$$

Martin does not define strains in space in his book, however, we can extend the same idea to space. A **strain** of ratio  $k$  about the  $X$ -axis in space (with  $YOZ$  plane as the fixed plane) can be represented by the following set of equations in Cartesian coordinate system,

$$\begin{cases} X' = kX \\ Y' = Y \\ Z' = Z \end{cases} \quad \text{Where} \quad k \neq 0$$



We see from the above definition that a strain in space is exactly a Hilbert dilatation when the “fixed direction” is chosen to be perpendicular to the “fixed plane”; we see further that the transformation demonstrated in section 2.1 is a strain of ratio  $a / b$  about

the Y-axis with the XOZ plane as the fixed plane.

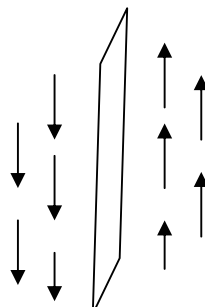
If we assume that the “fixed direction” described in Hilbert dilatation need not be perpendicular to the “fixed plane”, then we need to define a new transformation to fully understand Hilbert dilatation. This new kind of transformation is called a **shear**. Martin defines a shear in the plane as follows,

A **shear in the plane** about the X-axis is a transformation having the following equations,

$$\begin{cases} X' = X + kY \\ Y' = Y \end{cases} \quad \text{Where} \quad k \neq 0$$

Again, shear in space is not defined by Martin, but extending the same idea, a **shear in space** about the YOZ plane can be represented by

$$\begin{cases} X' = X \\ Y' = Y + k_1X \\ Z' = Z + k_2X \end{cases} \quad \text{Where} \quad k_1^2 + k_2^2 \neq 0$$



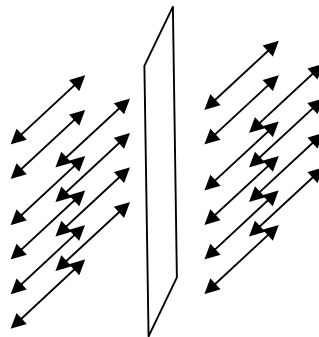
Shear in space

We see from the above definition that there is always a fixed plane in a shear in space.

In the above equations, the YOZ plane is the fixed plane of the shear.

With the definitions for strain and shear in space, I shall now give a set of equations that can represent Hilbert dilatation. In Cartesian coordinate system, Hilbert dilatation of ratio  $k$  with YOZ plane as the fixed plane can be represented by the following set of equations:

$$\left\{ \begin{array}{l} X' = kX \\ Y' = Y + k_1X \\ Z' = Z + k_2X \end{array} \right. \quad \text{Where} \quad k > 0, \text{ and } k \neq 1$$



Hilbert's dilatation

We see that in the above equations, when  $k_1 = k_2 = 0$ , it becomes a strain.

From the equations that represent a strain, a shear and a Hilbert dilatation, I derived the following theorem:

**Theorem 2.2-1: Hilbert dilatation is a product (composition) of a strain and a shear in space.**

I omit the proof.  $\square$

There is an important theorem relating strains and general linear transformations in space, namely,

**Theorem 2.2-2: A linear transformation is a product (composition) of strains.**

To see why Theorem 2.2-2 is true, here it becomes necessary to define clearly the following terms: “transformation”, “collineation”, “linear transformation”, and “affine transformation”.

**Definition I: A transformation** in space is a one-to-one correspondence from the set of points in space onto itself.

**Definition II: A collineation** is a transformation that transforms straight lines to straight lines.

**Definition III: A linear transformation** in the Cartesian coordinate system in space is any mapping having the following equations:

$$\left\{ \begin{array}{l} X' = aX + bY + cZ + p, \\ Y' = dX + eY + fZ + q \\ Z' = gX + hY + mZ + r \end{array} \right. \quad \text{Where} \quad \left| \begin{array}{ccc} a & b & c \\ d & e & f \\ g & h & m \end{array} \right| \neq 0$$

We see from this definition that, strains, shears and Hilbert dilatations are all linear transformations.

Note that the term “linear transformation” defined by Definition III is different from what we usually see in linear algebra.

**Definition IV: An affine transformation** is a collineation that preserves parallelism

among lines (Meaning that parallel straight lines are transformed to parallel straight lines under an affine transformation).

With the above four definitions, the following three theorems are stated in Martin's book.

Theorem IV: A collineation is an affine transformation; an affine transformation is a collieation. (Martin, p.167)

Theorem V: A linear transformation is an affine transformation; an affine transformation is a linear transformation. (Martin, p. 175)

Theorem VI: An affine transformation is a product of strains. (Martin, p.179) Although for Theorem VI Martin only gives proofs when all the transformations are plane transformations, but using similar arguments, it can be extended to transformations in space. Algebraically, an affine transformation in space can be represented by a  $3 \times 3$  invertible matrix. This matrix can always be factorized into a product of elementary matrices. Any one of the three types of elementary matrices is exactly a shear, a strain and a reflection, and it can be shown that a shear and a reflection is a composition of strains.

Theorem IV and V imply the fact that linear transformation, affine transformation and collineation are equivalent. Theorem 2.2-2 follows immediately from theorem VI and this fact. Despite the validity of Theorem 2.2-2, in the context of group of

transformations, the set of all strains does not form a group, while the set of all linear transformations forms a group. The reason why the set of all strains does not form a group is because this set does not satisfy the **closure property** of a group. The composite of two strains in space with two intersecting fixed planes is not a strain. However, I successfully proved the following theorem, which I shall state here without proof:

**Theorem 2.2-3:** The composition of two strains with parallel (or the same) fixed plane(s) is either a strain or a translation along the direction of the two strains.

As a summary, I end this section with the following remark on transformations in space.

**Remark 2.2:** Hilbert dilatation is a product of a strain and a shear in space. Affine transformations, collineations and linear transformations are equivalent transformations. A linear transformation is a product of strains. Since isometries, stretches, dilations, similarities, central similarities, strains, shears and Hilbert dilatations are all linear transformations, so each of them is a product of strains. In this regard, strains seem to be the most fundamental transformations among all linear transformations.

Since strains seem to be the most fundamental linear transformations, in the next section, I will explore the properties of strains.

## §2.3 Properties of strains

In this section, I shall explore the properties of strain transformations both in the plane and in space. Some of the properties discussed in this section will be useful in the proof presented in section 3.1.

### **Strains in the plane**

**Property P1:** Strains in the plane preserve collinearity and parallelism.

Property P1 says that, under any strains in the plane, straight lines are transformed into straight lines and parallel straight lines remain parallel. In previous section, we have already seen that a strain is a linear transformation, and a linear transformation is an affine transformation. Property P1 follows immediately from the definition of affine transformation.

**Property P2:** Strains in the plane preserve betweenness.

What I mean by Property P2 is that, under any strains, for all points lying on a common straight line, the distance between any two of them changes in the same ratio. In particular, if points  $P$ ,  $Q$  and  $R$  lie on the same straight line and  $P$  is the midpoint of the other two, then  $P'$  is always the midpoint of  $Q'$  and  $R'$  under any strains. To see this

property, we build up a Cartesian coordinate system in the plane such that X-axis is parallel to the direction of the strain, and Y-axis coincides with the fixed straight line of the strain. Take any straight line in the plane, suppose it has a gradient of  $\mathbf{k}$ . then for any two points on this straight line with X-coordinates equal to  $x_1$  and  $x_2$ , the distance between them is

$$\mathbf{D}(x_1, x_2) = (x_1 - x_2) \sqrt{(1+k^2)}$$

After the strain of ratio  $\mathbf{a}$ ,

$$\mathbf{D}'(x_1, x_2) = \mathbf{a} (x_1 - x_2) \sqrt{(1+k^2)}$$

So after the strain, the distance between  $x_1$  and  $x_2$  changes by a ratio of

$$\mathbf{D}'(x_1, x_2) / \mathbf{D}(x_1, x_2) = [\mathbf{a}\sqrt{(1+k^2)}] / \sqrt{(1+k^2)}$$

Since factor  $\mathbf{a}$  is constant and  $\mathbf{k}$  is the same for all points lying on the straight line, the result thus follows.

**Property P3:** Strains in the plane preserve the type of second order plane curves.

For this property I shall present the proof for the case that under a strain, an ellipse will always remain as an ellipse (or a circle). Using the previous Cartesian coordinate system, suppose an ellipse having the following general equation:

$$\mathbf{A}X^2 + \mathbf{B}Y^2 + \mathbf{C}XY + \mathbf{D}X + \mathbf{E}Y + \mathbf{F} = \mathbf{0}$$

Let

$$\Delta = \begin{vmatrix} A & \frac{1}{2}C & \frac{1}{2}D \\ \frac{1}{2}C & B & \frac{1}{2}E \\ \frac{1}{2}D & \frac{1}{2}E & F \end{vmatrix}, \quad J = \begin{vmatrix} A & \frac{1}{2}C \\ \frac{1}{2}C & B \end{vmatrix}, \quad I = A + B,$$

$$K = \begin{vmatrix} A & \frac{1}{2}D \\ \frac{1}{2}D & F \end{vmatrix} + \begin{vmatrix} B & \frac{1}{2}E \\ \frac{1}{2}E & F \end{vmatrix},$$

For the equation to be an ellipse type, if and only if,

$$\Delta \neq 0$$

$$J > 0 \text{ and}$$

$$\Delta/I < 0$$

After a strain of ratio  $a$  along the X-axis direction, the curve can be represented by

$$a^2AX'^2 + BY'^2 + aCX'Y' + aDX' + EY' + F = 0$$

I shall now shall that the corresponding conditions for the above equation to be an ellipse also hold, namely

$$\Delta' \neq 0$$

$$J' > 0 \text{ and}$$

$$\Delta'/I' < 0$$

For this purpose we expand  $\Delta$ ,  $J$ ,  $\Delta'$  and  $J'$ , we see that

$$\Delta = ABF + (1/4)CDE - (1/4)AE^2 - (1/4)FC^2 - (1/4)BD^2$$

$$J = AB - (1/4)C^2$$

$$\Delta' = a^2ABF + (1/4)a^2CDE - (1/4)a^2AE^2 - (1/4)a^2FC^2 - (1/4)a^2BD^2$$

$$J' = a^2AB - (1/4)a^2C^2$$

So we have

$$\Delta' = a^2\Delta \text{ and } J' = a^2J$$

By our assumption  $a$  is nonzero, so  $\Delta \neq 0$  and  $J > 0$  imply  $\Delta' \neq 0$  and  $J' > 0$ .

Note that since

$$\mathbf{J} = \mathbf{AB} - (1/4)\mathbf{C}^2 > 0$$

$\mathbf{A}$  and  $\mathbf{B}$  must be of the same sign, and since

$$\mathbf{I} = \mathbf{A} + \mathbf{B}$$

$$\mathbf{I}' = \mathbf{A}' + \mathbf{B}' = a^2\mathbf{A} + \mathbf{B}$$

So  $\mathbf{I}$  and  $\mathbf{I}'$  must be of the same sign, and we know  $\Delta' = a^2\Delta$ , therefore  $\Delta/\mathbf{I} < 0$  implies  $\Delta'/\mathbf{I}' < 0$ . So all the three conditions still hold after a strain.  $\square$

It can be proved in a similar way that in general, under any strain in the plane, hyperbolas will be transformed into hyperbolas, parabolas will be transformed into hyperbolas, so strain in the plane preserves the type of second order plane curves.

**Property P4:** Strains in the plane preserve concurrency and tangency.

If a straight line is tangent to an ellipse in the plane, after a strain, the ellipse is transformed into a new ellipse and the straight line a new straight line, Property P4 says that, this new straight line must be tangent to the new ellipse. Property P4 also says that if 3 straight lines are concurrent in the plane, they will always remain three concurrent straight lines under any strains in the plane. These properties follow from P3 and the fact that a strain (a linear transformation) is a mapping of points both one-to-one and onto.

Here I present an interesting example applying the idea of Property P4. I try to derive

the equation of a straight line tangent at a given point on a given ellipse by transforming the ellipse into a circle. The problem is shown below:

Suppose we have an ellipse in the plane having the following equation

$$X^2/a^2 + Y^2/b^2 = 1$$

What is the equation of the tangent line to this ellipse through a give point  $P(x_0, y_0)$  on the ellipse?

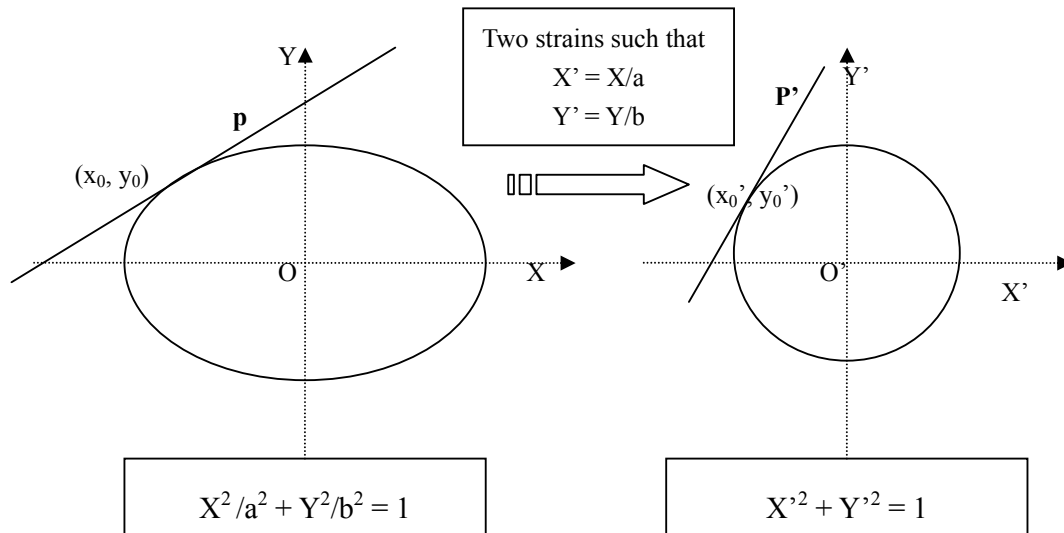


Figure 1.4-1

I solve this problem using strains. Suppose we keep the Y-axis fixed and do a strain to the X-axis such that  $X' = X/a$ . We then keep the X-axis fixed and do a strain to the Y-axis such that  $Y' = Y/b$ . We see that the ellipse in the original plane has become a circle in our new plane after the two strains. The circle has an equation of  $X'^2 + Y'^2 = 1$ .

Suppose the in the original plane,  $p$  is the straight line tangent to the ellipse at point  $(x_0, y_0)$ ,

$y_0$ ), then by our Property P1 and P4,  $\mathbf{p}$  must be transformed into a new straight line tangent to the circle at a point  $(x_0', y_0')$  where  $x_0' = x/a$ ,  $y_0' = y/b$ .

Now any straight line tangent to a circle must be perpendicular to the straight line connecting the center of the circle and the point of contact. So if the gradient of  $\mathbf{p}$  is  $\mathbf{k}$ ,  $\mathbf{k}$  must satisfy  $\mathbf{k} (y_0' / x_0') = -1$ , and hence  $\mathbf{k} = -(x_0' / y_0')$ .

Since  $\mathbf{p}$  pass through the point  $(x_0', y_0')$ , so the equation of  $\mathbf{p}'$  can be written as

$$(Y' - y_0') / (X' - x_0') = -(x_0' / y_0')$$

Now if we do the reverse of the two strains in the plane, or in other words if we now substitute back  $X' = X / a$  and  $Y' = Y / b$ , we will get the equation of  $\mathbf{p}$  in the original plane, which is

$$y_0 Y / b^2 + x_0 X / a^2 = 1$$

This is exactly the correct equation we want! The above result, to some extend, verifies the validity of our Property P1, P3 and P4.□

Anyone with elementary projective geometry knowledge may notice from our Property P1 and P4 that, the idea of strains are closely related to the idea of perspectives in Projective Geometry. Since strains always transform straight lines to straight lines and they preserve tangency and concurrency, any projective configurations that can be transformed into each other under strains are essentially isomorphic configurations in

the context of Projective Geometry.

For example, if we can proof Brianchon's Theorem in the case that if the 6 sides of a hexagon touch a circle, the three diagonals of the hexagon must be concurrent, we can immediately extend this theorem to the cases for ellipses, namely if the 6 sides of a hexagon touch an ellipse, the three diagonals of the hexagon must also be concurrent. To see this result, we simply transform the ellipse to a circle under a number of strains, (in fact in this case one single strain is always enough.), by Brianchon's Theorem for the circle case, the 3 diagonals after the strains must be concurrent. We then do the reverse transformations to get back our original ellipse, while it can be shown that the reverse transformation of a strain is also a strain, by P4, the result follows.

**Property P5:** Any two intersecting straight lines can be transformed into two perpendicular straight lines by one strain in the plane.

Property P5 is easy to see if we choose the fixed straight line of the strain to be the angle bisector of the two straight lines. In fact Martin states a much stronger property similar to Property P5: given  $\triangle ABC$  and  $\triangle DEF$ , there is a unique affine transformation that transforms  $\triangle ABC$  onto  $\triangle DEF$ . (Martin, p.176)

## **Strains in space**

I shall follow the same way as in the case of strains in the plane, listing out explicitly the properties of strains in space in this section.

**Property S1:** Strains in space preserve collinearity, coplanarity and parallelism.

This property says that strains in space transform straight lines into straight lines, planes into planes; parallel straight lines or planes remain parallel under any strains in space.

**Property S2:** Strains in space preserve betweenness.

Analogous to Property P2, Property S2 says that under any strain in space, for all points lying on a common straight line, the distance between any two of them change in the same ratio. In particular, if points P, Q and R lie on the same straight line and P is the midpoint of the other two, then P' is always the midpoint of Q' and R' under any strains.

Property S2 can be shown using a similar proof presented under Property P2.

**Property S3:** Strains in space preserve the type of second order surfaces.

Property S3 says that, an ellipsoid in space will always remain as an ellipsoid under any

strains in space; a hyperboloid of one sheet will always remain as a hyperboloid of one sheet under any strains in space, and same for other types of quadrics.

**Property S4:** Strains preserve concurrency and tangency in space.

**Property S5:** Any two intersecting planes can be transformed into two perpendicular planes by one strain.

Property S5 is easy to see if we choose the fixed plane of the strain to be the dihedral angle bisector of the two given intersecting planes.

All the properties of strains in space bear analogous ideas from corresponding properties of strains in the plane, and the proofs are similar, here I shall only present a proof for Property S3, and for the case when the quadratic surface is a hyperboloid of one sheet.

Given a general quadratic equation in three variables,

$$aX^2+bY^2+cZ^2+2fYZ+2gZX+2hXY+2pX+2qY+2rZ+d=0,$$

Let

$$e = \begin{bmatrix} a & h & g \\ h & b & f \\ g & f & c \end{bmatrix} \quad \text{and} \quad E = \begin{bmatrix} a & h & g & p \\ h & b & f & q \\ g & f & c & r \\ p & q & r & d \end{bmatrix};$$

For the equation to be a representation of a hyperboloid of one sheet, if and only if the

following 3 conditions hold,

Condition 1: **Rank( $e$ ) = 3**

Condition 2: **Det( $E$ ) > 0**

Condition 3: The nonzero eigenvalues of  $e$  are not all of the same sign.

(Depending on whether the above conditions are satisfied or not, a general second order equation with three variables can represent in total 17 different types of quadratic surfaces including imaginary surfaces. For example, if in the above three conditions, condition 3 is changed to be its negation, then the equation will represent an imaginary ellipsoid.)

I shall show that after a strain of ratio  $k$  ( $k \neq 0$ ) with the YOZ plane as the fixed plane, the above three conditions still hold. After the strain, the original equation becomes

$$k^2 aX^2 + bY^2 + cZ^2 + 2fYZ + 2kgZX + 2hkXY + 2pkX + 2qY + 2rZ + d = 0,$$

Suppose the corresponding  $e$  and  $E$  now become  $e'$  and  $E'$ , where

$$e' = \begin{pmatrix} k^2 a & kh & kg \\ kh & b & f \\ kg & f & c \end{pmatrix} \quad \text{and} \quad E' = \begin{pmatrix} k^2 a & kh & kg & kp \\ kh & b & f & q \\ kg & f & c & r \\ kp & q & r & d \end{pmatrix}$$

It can be calculated from above that

$$\mathbf{Det}(e') = k^2 \mathbf{Det}(e) \text{ and}$$

$$\mathbf{Det}(E') = k^2 \mathbf{Det}(E).$$

Condition 1. Since

$$\mathbf{Rank}(e) = 3 \text{ implies } \mathbf{Det}(e) \neq 0$$

and by our assumption  $k \neq 0$ , it follows that

$$\mathbf{Det}(e') = k^2 \mathbf{Det}(e) \neq 0$$

$$\mathbf{Det}(e') \neq 0 \text{ implies } \mathbf{Rank}(e') = 3$$

Condition 2:

$$\mathbf{Det}(E) > 0 \text{ and } k^2 > 0 \text{ imply}$$

$$\mathbf{Det}(E') = k^2 \mathbf{Det}(E) > 0$$

Condition 3: We need some theorems in linear algebra to see why condition 3 holds after the strain. They are:

Theorem A: A square matrix A is invertible if and only if  $\lambda = 0$  is not an eigenvalue of A.

(Anton p.343)

Theorem B: If A is a symmetric matrix, then the eigenvalues of A are all real numbers.

(Anton p.358 & p.526)

Theorem C: A symmetric matrix A is positive definite if and only if all the eigenvalues of A are positive. (Anton p.450)

Theorem D: A symmetric matrix A is positive definite if and only if all the determinant of every principal submatrix is positive. (Anton p.451)

From Theorem C and D, the following theorem can be deduced.

Theorem E: A symmetric matrix has both positive and negative eigenvalues if and only if the determinants of its principal submatrices have both positive and negative values.

Since both matrix  $e$  and matrix  $e'$  have a rank of 3, so both of them are invertible, we see from Theorem A that,  $\lambda=0$  is not an eigenvalue of either  $e$  or  $e'$ . Since both matrix  $e$  and matrix  $e'$  are symmetric matrices, we see from Theorem B that the eigenvalues of both  $e$  and  $e'$  are real values. So now we know that both  $e$  and  $e'$  has 3 nonzero real eigenvalues.

It can be shown that the determinants of the principal submatrices of  $e'$  are  $k^2(>0)$  times the determinants of corresponding principal submatrices of  $e$ , so the strain does not change the signs of the determinants of the principal submatrices of  $e$ . From Theorem E, it follows that if the nonzero eigenvalues of  $e$  are not all of the same sign, then the nonzero eigenvalues of  $e'$  are not all of the same sign, too. Hence we see that Condition 3 holds under the strain.

Since all the 3 conditions still hold after the strain, we have proved that under any strains in space, a hyperboloid of one sheet will remain as a hyperboloid of one sheet.  $\square$

Intuitively, since a hyperboloid of one sheet is a doubly ruled surface which contains two families of straight lines and infinitely many ellipses on it, and since strains in

space always change straight lines into straight lines, ellipses into ellipses, it can be imagined that, any strains in space will transform a hyperboloid of one sheet into a new quadratic surface that still contains two families of straight lines and infinitely many ellipses on it. The only quadratic surface having these properties is the hyperboloid of one sheet.

As have discussed in section 2.2, a linear transformation is a product of strains, so it is concluded here that all the properties of strains listed out in this section are also true for any other linear transformation. Since Hilbert dilatation is a linear transformation, so Hilbert dilatation preserves the type of a quadratic surface in space, and this explains the remarks given at the end of section 2.1.

## Chapter III

# Geometry and the Imagination

### §3.1 From skew lines to a hyperboloid of one sheet

On page 14 of Hilbert's book, he presented a method for generating a hyperboloid of one sheet from 3 given straight lines in space which are mutually skew and are not parallel to a common plane:

Let  $\mathbf{p}$ ,  $\mathbf{q}$  and  $\mathbf{r}$  be the 3 given straight lines, we construct all the straight lines which have a common point with each of the three lines. To do this, we choose a point  $\mathbf{P}$  on  $\mathbf{p}$ , take the intersection of the plane containing  $\mathbf{P}$  and  $\mathbf{q}$  with the plane containing  $\mathbf{P}$  and  $\mathbf{r}$ , hence the straight line of intersection is what we want. By varying the position of  $\mathbf{P}$ , we will get all the straight lines that intersecting all 3 given lines. All these straight lines that we have just constructed make up a hyperboloid of one sheet.

Hilbert argues that since a hyperboloid of one sheet consists of two families of straight lines, and these straight lines are arranged such a way that every line of one family has a point in common with every line of the other family and any two lines of the same family are mutually skew, if we take the given three skew straight lines  $\mathbf{p}$ ,  $\mathbf{q}$  and  $\mathbf{r}$  to be three lines coming from the same family of a hyperboloid of one sheet, then any straight

line that intersects all the 3 given lines must be on the same surface, because no straight line not lying in the surface can intersect a quadratic surface at more than two points.

A careful reader will soon notice that in Hilbert's arguments, he actually made an assumption which is not so easy to see why, that is,

For any 3 given straight lines in space which are mutually skew and are not parallel to a common plane, there always exists a hyperboloid of one sheet such that this hyperboloid of one sheet contains the 3 given straight lines.

Hilbert indeed made the assumption without a proof. In fact, he stated without proof on page 15 in his book that

“Three skew straight lines always define a hyperboloid of one sheet, except in the case where they are all parallel to one plane (but not to each other). In this case they determine a hyperbolic paraboloid.”

In this section I will present a proof for the following theorem:

**Theorem 3.1** For any three straight lines which are mutually skew and are not parallel to a common plane, there always exist a hyperboloid of one sheet containing these three lines.

Denote the three straight lines with  $p$   $q$   $r$ . I will prove the above theorem in 4 steps.

**Step 1.** Construct a space hexagon. This hexagon has the following properties.

1.  $\mathbf{p}$   $\mathbf{q}$   $\mathbf{r}$  pass through 3 alternating sides of the hexagon. (By “3 alternating sides of the hexagon” I mean 3 sides of the hexagon among which no two are adjacent.)
2. Any two opposite sides of this space hexagon are parallel and are of equal length.

To construct the desired hexagon, we first construct a plane  $S_1$  containing  $\mathbf{p}$ , and a plane  $S_2$  containing  $\mathbf{q}$  such that  $S_1 \parallel S_2$  (Figure 3.1-1). Note that such  $S_1, S_2$  always exist since  $\mathbf{p}$   $\mathbf{q}$  are two skew straight lines in space.

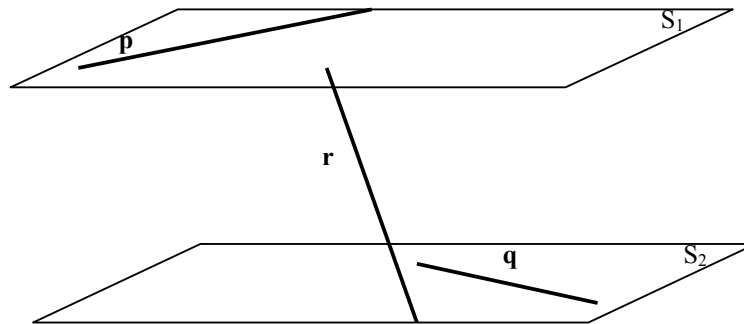


Figure 3.1-1

Claim: the third straight line  $\mathbf{r}$  must intersect both  $S_1$  and  $S_2$ . If not, then  $\mathbf{r} \parallel S_1 \parallel S_2$ , and we can always find a plane parallel to the three given lines, which contradicts our assumption that such plane does not exist, hence the claim. Now since the claim is true, suppose  $\mathbf{r}$  intersect both  $S_1$  and  $S_2$  at points A, B respectively (Figure 3.1-2)

We then draw a straight line on  $S_1$  through A parallel to  $\mathbf{q}$ , since  $\mathbf{p}$   $\mathbf{q}$  are skew, the line we draw must intersect  $\mathbf{p}$ , for otherwise it will imply that  $\mathbf{p} // \mathbf{q}$ . Denote the point of intersection with F. Similarly we draw a straight line on  $S_2$  through B parallel to  $\mathbf{p}$ , it intersects  $\mathbf{q}$  at a point, denote it with C.

Suppose we now construct a plane  $S_3$  which contains  $\mathbf{p}$  and parallel to  $\mathbf{r}$ , by a similar argument as before,  $\mathbf{q}$  must intersect with  $S_3$ , denote the point of intersection with D.

Draw the straight line on  $S_3$  through D and parallel to  $\mathbf{r}$ . This line intersects  $\mathbf{p}$ , denote the point of intersection E.

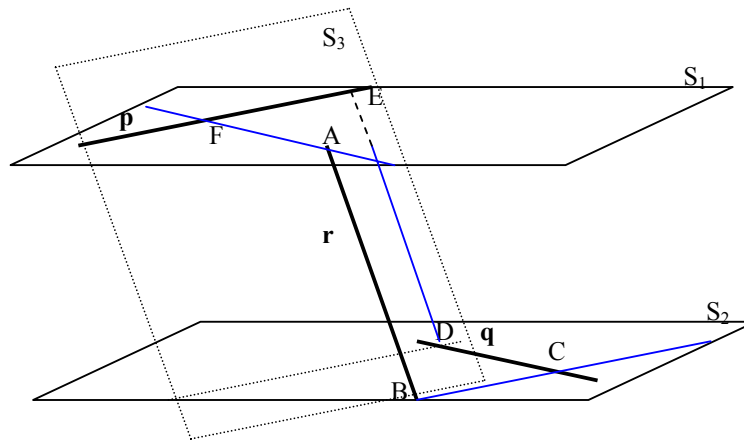


Figure 3.1-2

Now we see that ABCDEF form a space hexagon, with  $\mathbf{p}$   $\mathbf{q}$   $\mathbf{r}$  pass through 3 alternating sides of the hexagon. We see furthermore that each pair of opposite sides of this hexagon are parallel.

Observe that the two opposite side AB and DE are parallel straight line segments cut by two parallel planes, thus they must be equal in length. So we have

$$AB = DE$$

Using a similar argument,

$$BC = EF \text{ and } CD = FA$$

Thus the space hexagon ABCDEF we have constructed satisfies the two conditions.

Now there is another interesting fact about the space hexagon that we have just constructed, viz. the three diagonals of this space hexagon are concurrent.

To see why this is so, we connect CF BE, two of the three diagonals of the space hexagon (Figure 3.1-3). Now since the two sides BC and EF are parallel and equal in length, BCEF must form a parallelogram, and hence CF and BE intersects at point, denote this point with O, we have  $BO = EO$  and  $CO = FO$ .

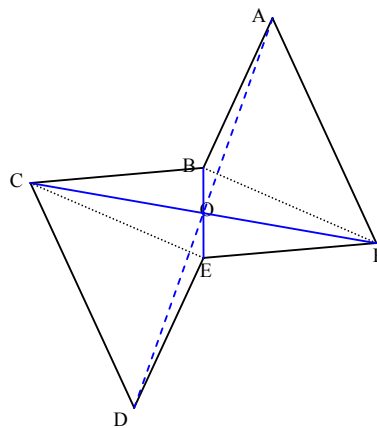


Figure 3.1-3

We now consider the two opposite sides AF and CD, using a similar argument we see that the third diagonal AD must intersect CF at the same point O. In other words, the three diagonals of the space hexagon are concurrent at a point O, and furthermore,  $AO = OD$ ,  $BO = OC$ ,  $CO = OF$ .

**Step 2.** By applying transformations of strains in space, transform the six points ABCEDF to positions of the six vertices of a regular octahedron.

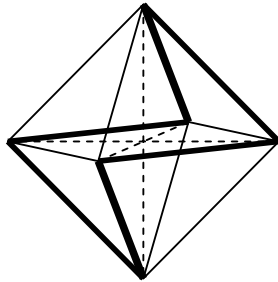


Figure 3.1-4

A regular octahedron is shown in Figure 3.1-4. It has six vertices and eight faces. Every face is an equilateral triangle. The three diagonals of a regular octahedron are mutually perpendicular and are equal in length. Note that a space hexagon is highlighted in the figure. The goal of step 2 is to transform the space hexagon constructed in step 1 to this shape.

In order to transform the six points ABCDEF to the positions of the 6 vertices of an octahedron by strains in space, we consider the positions of the three diagonals of the

space hexagon  $ABCEDF$ . From Property  $S7$  in section 2.3 we know that under any strains in space, point  $O$  will always remain at the center of  $AD$   $CE$  and  $BF$ , so if, by applying strains in space, we can transform the three diagonals into some new positions such that they are mutually perpendicular and  $AD = CE = BF$ , then we are through.

To this end, we first transform  $AD$  and the plane containing  $BCEF$  into perpendicular positions. Denote the plane containing  $BCEF$  with  $S_4$  (Figure 3.1-5). If  $AD$  is perpendicular to  $S_4$ , then skip the following step.

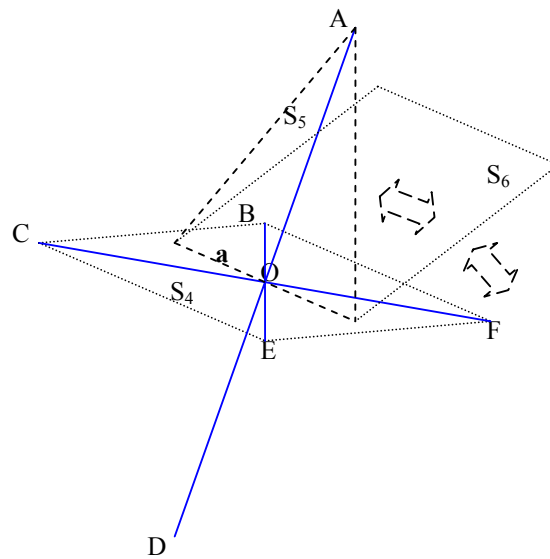


Figure 3.1-5

Assume  $AD$  is not perpendicular to  $S_4$ . We draw on  $S_4$  a straight line  $\mathbf{a}$  through point  $O$  and perpendicular to  $AD$ . Note that such  $\mathbf{a}$  always exists and it is the intersection of  $S_4$  and the plane through point  $O$  and perpendicular to  $AD$ .

By our construction  $\mathbf{a}$  intersects AD at point O, thus  $\mathbf{a}$  and AD are coplanar. Denote the plane containing AD and  $\mathbf{a}$  with  $S_5$ . Apparently  $S_5$  and  $S_4$  intersect in  $\mathbf{a}$ , so by Property  $S_6$  discussed in section 2.3,  $S_4$  and  $S_5$  can be transformed into two perpendicular plane. And the way to do this is as follows, we take a plane  $S_6$  through  $\mathbf{a}$  such that it makes the same dihedral angle  $\theta$  with  $S_4$  and  $S_5$ ,  $\theta$  must be greater than 0 and less than 90 degree. We then choose  $S_6$  to be the fixed plane and apply a strain in space about this plane with a ratio equal to  $\text{Cot}(\theta)$ , it can be shown that under this strain,  $S_4$  and  $S_5$  will be transformed into two perpendicular planes.

It can further be proved that  $\mathbf{a}$  and AD remain perpendicular in the process. Because in the process of the strain, the projection of AD on  $S_6$  will always remains unchanged, and it can be deduced from this that AD and  $\mathbf{a}$  remain perpendicular under the above transformation of strain.

We now look at the new positions of the figures after we applied the strain in space. Since now the plane containing AD and  $\mathbf{a}$  is perpendicular to  $S_4$ , and AD is perpendicular to  $\mathbf{a}$ , the intersection of  $S_4$  and  $S_5$ , it follows that now AD is perpendicular to  $S_4$  (Figure 3.1-5).

In the new figure, we draw the angle bisector  $\mathbf{b}$  of  $\angle BOC$  on  $S_4$ , suppose  $\mathbf{b}$  makes an angle  $\theta'$  with either OC or OB. Since  $\mathbf{b}$  has a common point O with AD, they are

coplanar. Denote the plane containing AD and  $\mathbf{b}$  with  $S_7$ . AD is perpendicular to  $S_4$  necessarily implies the fact that  $S_7$  is perpendicular to  $S_4$ .

We then do another strain in space. This time we choose  $S_7$  as the fixed plane, and  $\text{Cot}(\theta')$  as the strain ratio, it can be proof that after this transformation, BE and CF become perpendicular, and in the process, AD always remain perpendicular to  $S_4$ . By now all the three diagonals AD BE and CF become mutually perpendicular, the thing remained is to transform them into equal length. But this remaining task is easy to do.

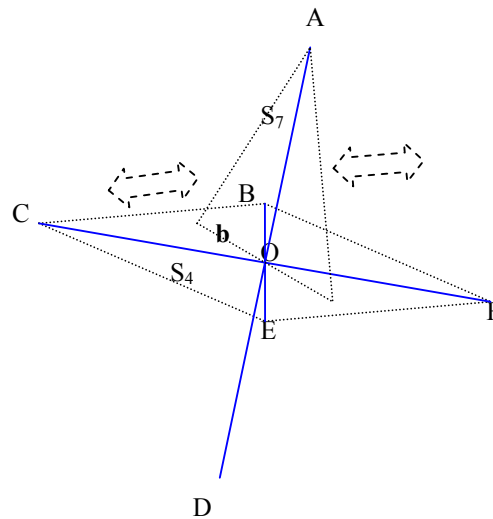


Figure 3.1-6

We first choose the plane containing AD and BE to the fixed plane, and apply a strain in space with ratio equal to the AD/CF, then CF is transformed to have the same length with AD. We then choose the plane containing AD and CF to be the fix plane, and do a

strain with ratio equal to  $AD/BE$ , obviously this time the length of  $AD$  and  $CF$  remain unchanged since they are on the fixed plane, and  $BE$  become of equal length to  $AD$  and  $CF$ .

With above all done, the space hexagon we have constructed in step one now can fit on a regular octahedron as shown in Figure 3.1-7.

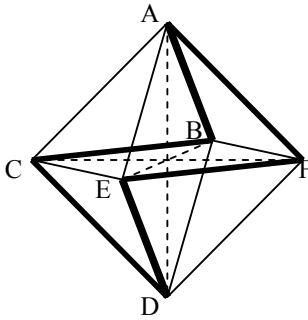


Figure 3.1-7

**Step 3.** Claim: There is a hyperboloid of revolution of one sheet which contains the 3 straight lines passing through  $AB$ ,  $CD$  and  $EF$  shown in Figure 3.1-7.

To see this, we take the center of the equilateral triangle  $ACE$ , denote this point with  $G$  (Figure 3.1-8). We then take the center of the equilateral triangle  $BDF$ , denote this point with  $H$ . Connect  $GH$ .

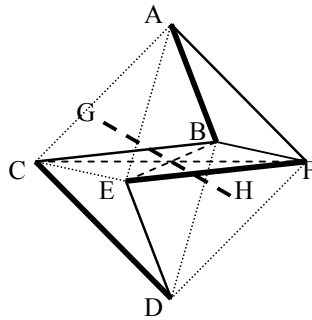


Figure 3.1-8

Now if we rotate the regular octahedron about the straight line passing through GH, by the highly symmetrical nature of a regular octahedron, we see that the three sides AB, CD and EF can be brought onto each other in the motion of rotation!

In section 1.2 we have seen that if we rotate a straight line in space about an axis skew to it, we will get a hyperboloid of revolution of one sheet. Now if we rotate the straight line containing the side AB about the axis GH (note that they are skew), we will get a hyperboloid of revolution of one sheet. Furthermore, the straight line containing CD or EF must also lie in the same hyperboloid since AB will at some moment coincide with both two sides in the process of rotation, hence the claim.

Same result for the other three alternating sides of the space hexagon, BC, DE and FA. It actually can be proved that the hyperboloid of revolution of one sheet generated by rotating any sides among the six about GH are the same, in other words, AB, BC, CD, DE, EF, FA, these six sides all lie in the surface.

**Step 4.** Conclusion: For any three straight lines in space which are mutually skew and are not parallel to a common plane, there always exists a hyperboloid of one sheet containing these three lines.

**Proof.** For any three straight lines in space which are mutually skew and are not parallel to a common plane, by our **Step 2** and **Step 3**, we can always transform them into positions such that they are contained in a hyperboloid of revolution of one sheet. Imagine now we construct the surface with the 3 straight lines in the surface in space. If we now do the reverse transformations of the four strains we had applied in space, by our Property S1, S4 in section 2.3, the hyperboloid of revolution must be transformed into a surface of a hyperboloid of one sheet which still contains the three straight lines. Since after the reverse transformations, the three straight lines are transformed back to their original positions, so we have seen that there always exists a hyperboloid of one sheet containing the three lines, hence the result.□

From discussions at the end of step 3 we actually can deduce that the hyperboloid of one sheet that contains **p q** and **r** must contain all the six sides of the space hexagon we constructed in step 1. As what I have pointed out in section 1.3, on a hyperboloid of one sheet, there are two families of straight lines, for any three straight lines from the same family, there is one and exactly one straight from the other family parallel to one of them and intersects the other two. Since in general, for any three skew straight lines in

space, the straight line parallel to one of them and intersecting the other two is unique, thus this straight line must also lie in the hyperboloid of one sheet defined by the three given skew lines. This explains why the six sides of the space hexagon are all contained in the hyperboloid of one sheet defined by  $\mathbf{p}$ ,  $\mathbf{q}$  and  $\mathbf{r}$ .

Of course by constructing arbitrary straight lines intersecting  $\mathbf{p}$ ,  $\mathbf{q}$  and  $\mathbf{r}$ , we can get infinitely many space hexagons such that the six sides of these hexagons all lie in the hyperboloid of one sheet defined by  $\mathbf{p}$ ,  $\mathbf{q}$  and  $\mathbf{r}$ . But these kinds of hexagons does not help in the above proof, because it is still hard to see what kind of strain transformations can bring the six sides of these irregular shapes to good positions, in this sense, the space hexagon we constructed in step 1 is certainly a wise one.

For the case when the three given straight lines are parallel to a common plane, they define a hyperbolic paraboloid. The construction of this hyperbolic paraboloid from the given three straight lines is similar to the hyperboloid of one sheet case: we construct all straight lines in space that intersect all three of the given straight lines. My proof for the hyperboloid of one sheet case can not be applied directly to solve the hyperbolic paraboloid case, because a hyperbolic paraboloid is not a surface of revolution, and cannot be obtained from a surface of revolution by strain transformations in space. However, algebraically, the hyperbolic paraboloid case is simpler to solve than the hyperboloid of one sheet, I will not present the analytical proof here.

### §3.2 The closest regular packing of spheres

In chapter 2 of Hilbert's book, in the study of space lattices, Hilbert mentioned an interesting problem: Suppose you have infinitely many spheres all of unit diameter, how can you arrange them in space to form a regular sphere packing with the highest density? The density of a packing of spheres can be understood as, within a sufficient large space, the ratio of the volume occupied by the spheres to the volume of the space.

We can construct such a packing layer by layer. To do this we first try to arrange the spheres on the same plane. The smartest way to do this is obviously to put 6 other spheres tangent to one at the center shown in Figure 3.2-1A, and then extend the same pattern in the plane, in this plane packing, every sphere is tangent to 6 others surrounding it. Evidently you cannot put more than 6 spheres all tangent to one at the center, so 6 is the best you can do. A not so smart way to do it is to arrange the spheres such that the centers of the spheres form unit squares as shown in Figure 3.2-1B.

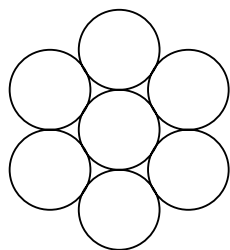


Figure 3.2-1A

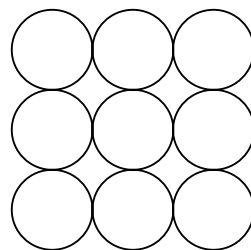


Figure 3.2-1B

We then extend the first layers into space. To do this we construct layers immediately above and below the first layers by adding spheres in the hollows of the first layers. We

can put one in every hollow (Figure 3.2-1D) of the layer shown in Figure 3.2-1B, but we can only choose alternating hollows in Figure 3.2-1A because there is insufficient room. In either case, all the other layers we extend from the first one are congruent with our first layer. There is only a shifting of position between them.

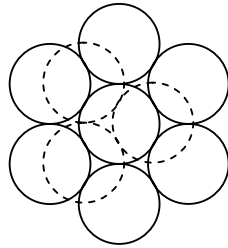


Figure 3.2-1C

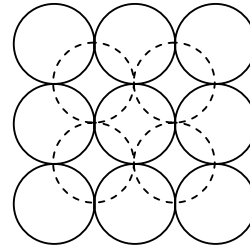


Figure 3.2-1D

In the case of Figure 3.2-1C, the kind of packing we get is usually called the face-centered hexagonal packing or the hexagonal close packing. If we choose proper hollows for each layer such that the centers of the spheres form a space lattice, the hexagonal close packing is also called a face-centered hexagonal lattice packing, while the one shown in Figure 3.2-2D is usually called a face-centered cubic lattice packing. Surprisingly, what seem to be two different resulting packings turn out to be identical, namely the face-centered hexagonal lattice packing described above is identical to the face-centered cubic lattice packing. It is just the different angles we look at the same structure that is deceiving. It is because of this that the hexagonal close packing mentioned above is also called a hexagonal cubic close lattice packing.

There are evidences that support the above mentioned fact. If we look at both the

face-centered hexagonal lattice packing and face-centered cubic lattice packing, in both packings, each sphere is tangent to 12 others surrounding it. In the hexagonal case, 6 in the same layer, 3 below and 3 above, while in the cubic case, 4 in the same plane, 4 below and 4 above.

However the surprising fact can best be understood by the structure of a regular octahedron. If we arrange unit regular octahedrons as shown in Figure 3.2-2 and extend the same pattern in space we will get a space lattice consisting of the vertices of the octahedrons.

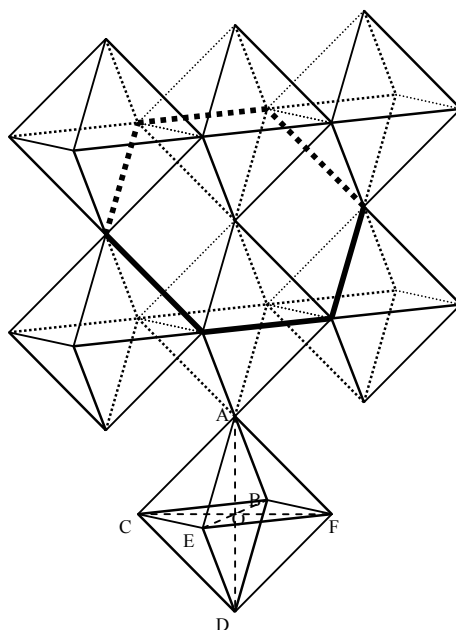


Figure 3.2-2

If we now put spheres of unit diameter at each vertex of the lattice we get, then the sphere packing is what we have constructed from face-centered hexagonal lattice

packing or face-centered cubic lattice packing. It becomes apparent in Figure 3.2-2 that if we look at the packing along the (3 different) directions of the three diagonals of the regular octahedrons, it appears to be a face-centered cubic lattice packing with horizontal layers perpendicular to our eyesight. If we look along the (4 different) directions perpendicular to the faces of the regular octahedrons, then the packing appears to be face-centered hexagonal lattice packing with horizontal layers perpendicular to our eyesight. So in this packing, there are three directions along which it appears to be a face-centered cubic lattice packing, while there are four different directions along which it appears to be a face-centered hexagonal lattice packing.

The distance between two adjacent layers (distance between the two planes containing the centers of the spheres of the two layers) for the face-centered cubic lattice packing equals the length of AO in Figure 3.2, and the value is  $(\sqrt{2})/2$ , and for the face-centered hexagonal lattice packing, it equals the distance between the plane containing ACE and the plane containing BDF, and the value is  $(\sqrt{6})/3$ . Note that the later value is bigger because layer-wise, the face-centered hexagonal lattice packing has bigger density, so the distance between two adjacent layers of the face-centered hexagonal lattice packing has to be greater in order for it to have the same density with the face-centered cubic lattice packing.

## **Bibliography**

- [1] Anton, Howard. Elementary Linear Algebra, Eighth Edition. John Wiley and Sons, Inc. New York, 2000.
- [2] Cederberg, Judith N. A Course in Modern Geometries. Springer-Verlag. New York 1989.
- [3] Eric W. Weisstein. "Quadratic Surface." From *MathWorld*--A Wolfram Web Resource. <http://mathworld.wolfram.com/QuadraticSurface.html>
- [4] Hilbert, D. and Cohn-Vossen, S. Geometry and the Imagination, Chelsea Publishing Company. New York, 1958.
- [5] Martin, George E. Transformation Geometry: An Introduction to Symmetry. Springer-Verlag. New York 1982.